

**ECE 4880**

**Fall 2016**

# **Chapter 7**

## **Architecture to Improve Linearity**

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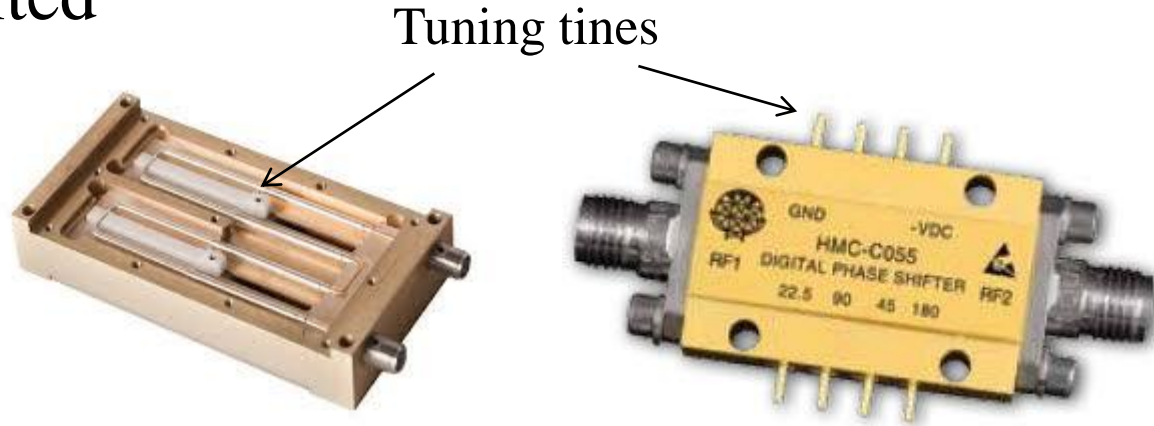
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# Goals

- Passive modules of
  - phase shifter
  - directional coupler
  - power divider
  - quadrature coupler
  - power/signal combiner
- Parallel combining
- Feedforward distortion cancellation
- Other feedback structures

# Phase Shifters

Passive: limited bandwidth



Active: nonlinearity



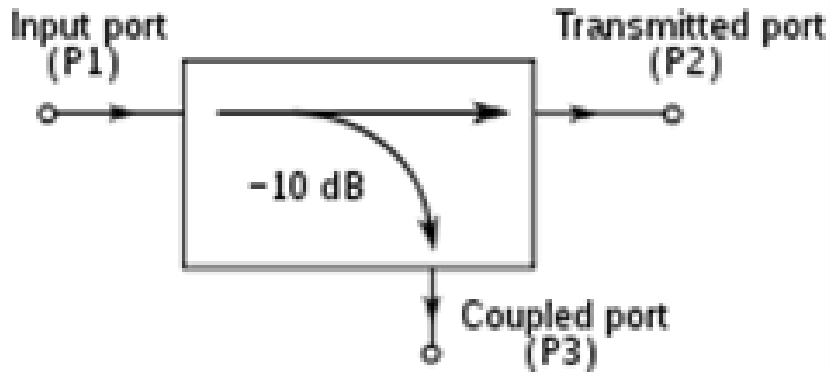
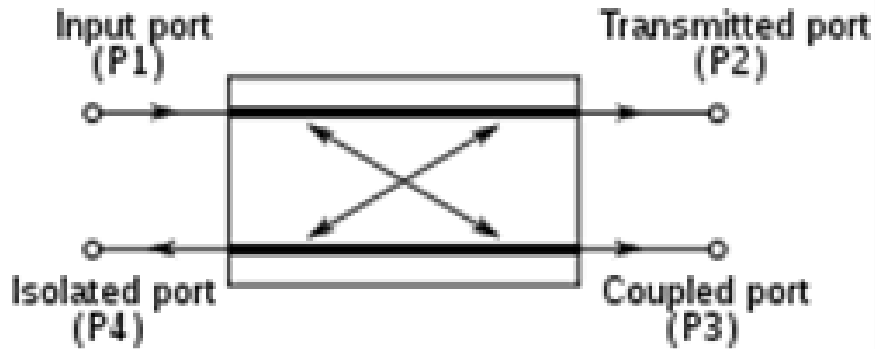
# Signal/Power Splitters



Passive: broad bandwidth

- Half power to Out1 and Out2 (3dB), or  $\frac{1}{\sqrt{2}}$  in voltage magnitude.
- Many splitters are bi-directional and can be used for combiner.

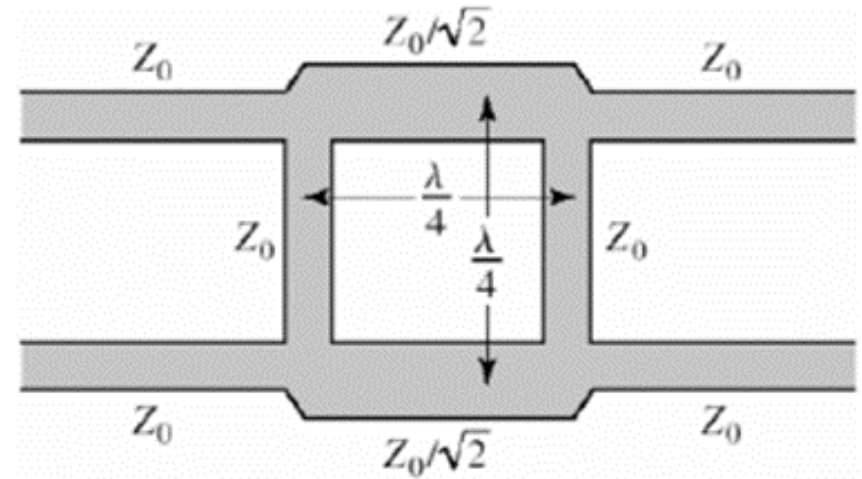
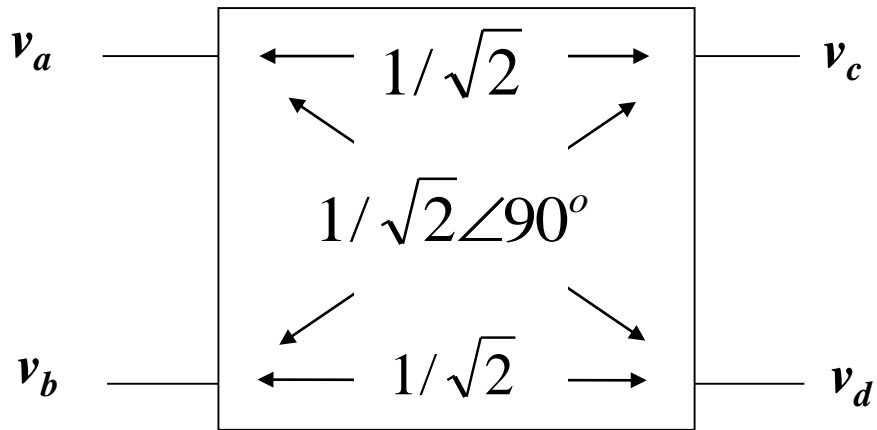
# Directional Couplers



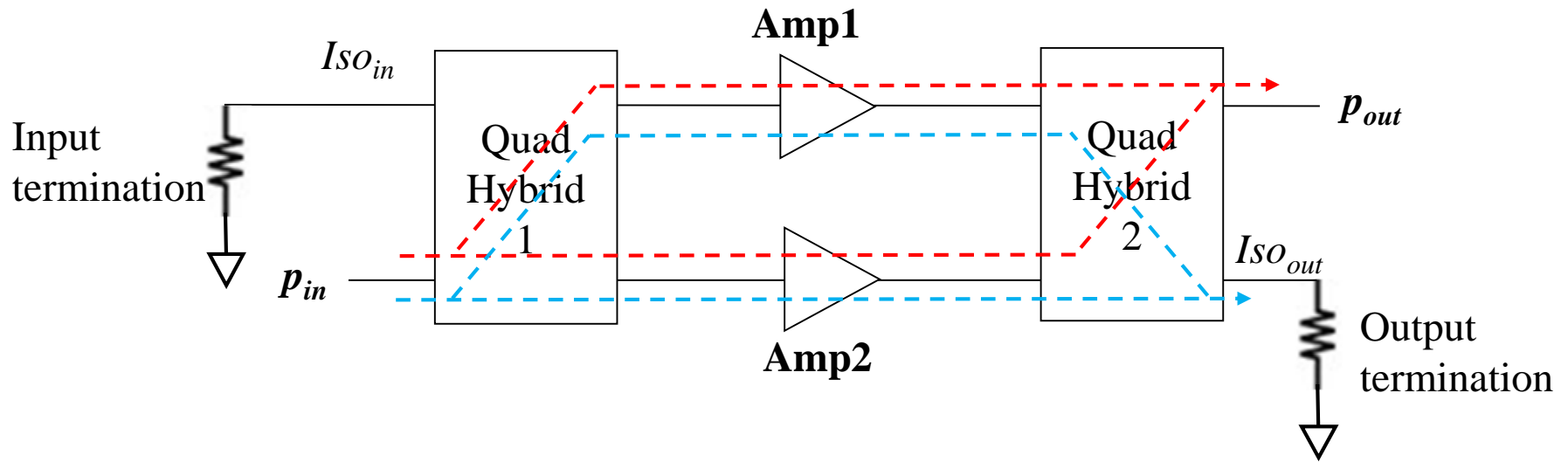
- $P1 \leftrightarrow P2$  about  $-0.5\text{dB}$
- $P1 \rightarrow P3$  about  $-10\text{dB}$
- $P2 \rightarrow P3$  about  $-50\text{dB}$

Passive: broad  
bandwidth

# Quadrature Hybrid Couplers (90°)

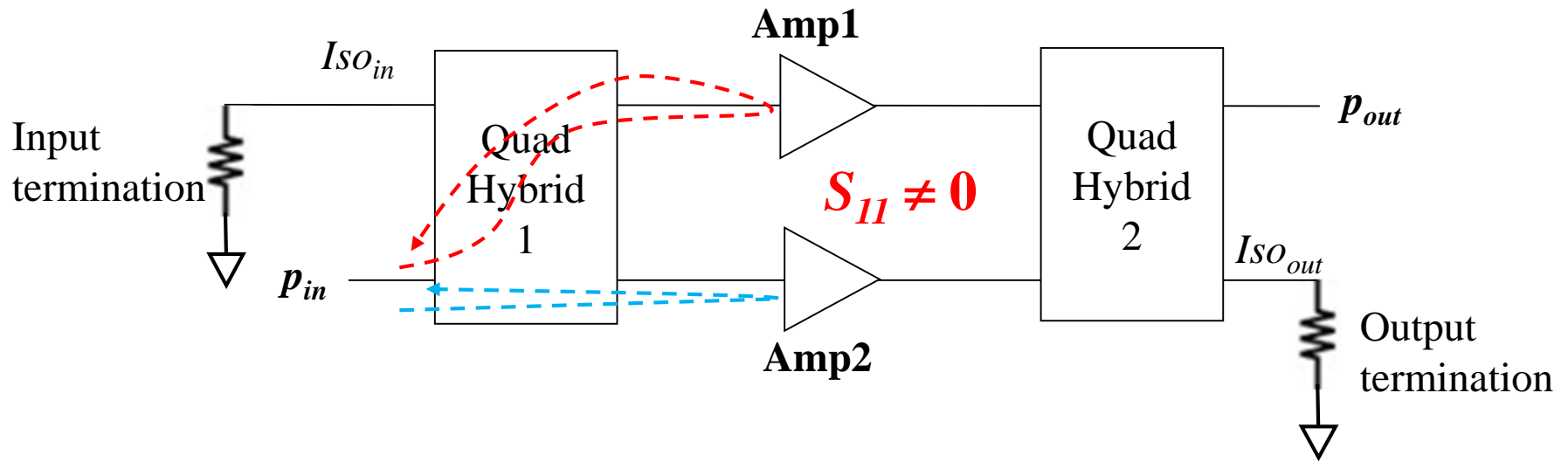


# Parallel Combining by Quad Hybrid



- $p_{in} \rightarrow p_{out}$ ; both paths  $90^\circ$  shift: in phase.
- $p_{in} \rightarrow I_{SO_{out}}$ ; one path  $0^\circ$  shift and the other  $180^\circ$ : out of phase.
- Amp1 and Amp2 shares the power amplification to generate the same  $p_{out}$ , but have 3dB lower input  $\Rightarrow$  3dB lower in  $p_{outIM2}$  and 6dB lower  $p_{outIM3}$

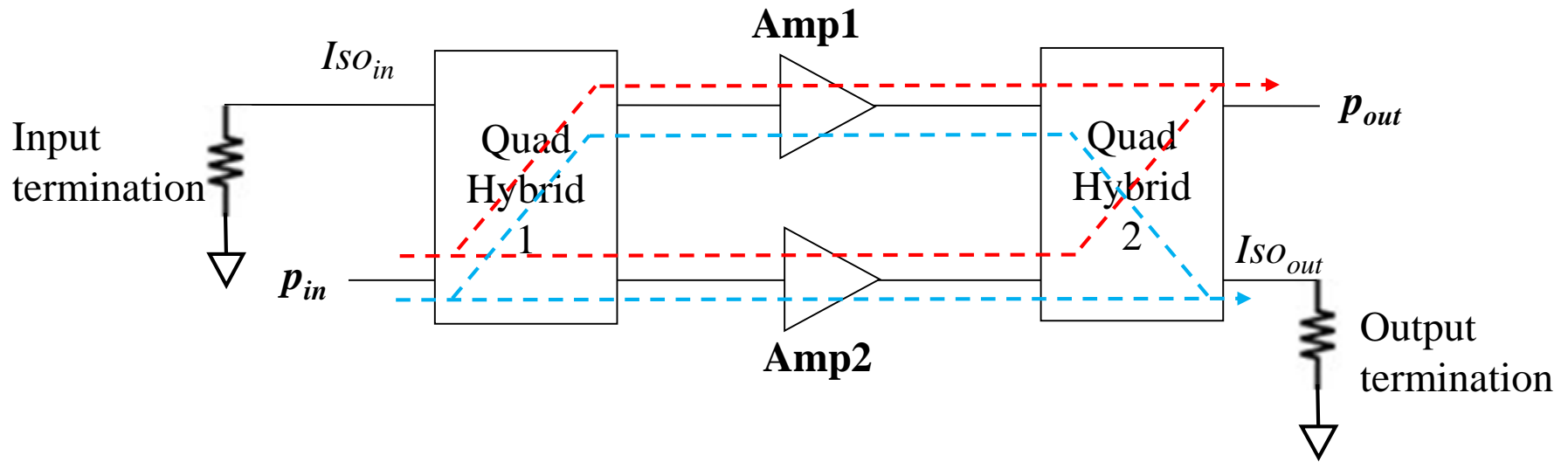
# Impedance Matching in Quad Hybrid



- $p_{in} \rightarrow \text{Amp1} \rightarrow p_{in}$ ;  $180^\circ$  shift
- $p_{in} \rightarrow \text{Amp2} \rightarrow p_{in}$ ;  $0^\circ$  shift: out of phase.
- If Amp1 and Amp2 have mismatched impedance to  $Z_0$ , as  $Z_{in1} = Z_{in2}$ , the reflection to  $p_{in}$  will be cancelled, and NO jitter to  $p_{in}$ ! (Where does the reflective power go?)
- How about the output impedance for Amp1 and Amp2?
- $I_{SO_{in}}$  and  $I_{SO_{out}}$  can dissipate non-match energy and for debugging



# H2 and H3 in Quad Hybrid

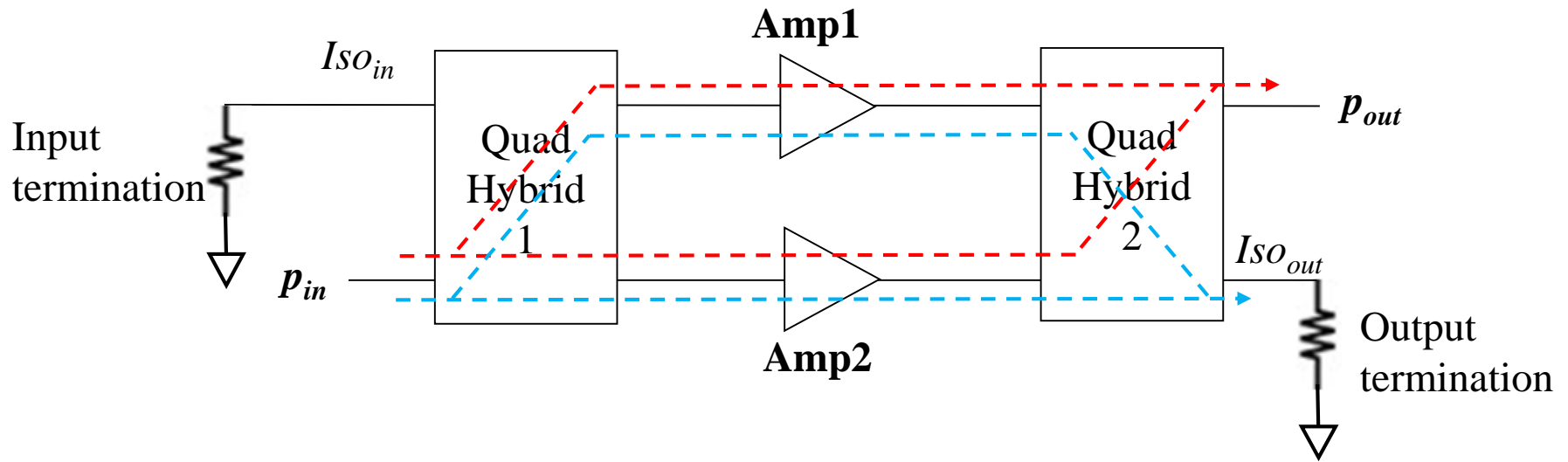


- $p_{in} \rightarrow Amp2 \rightarrow p_{out}$ :

$$v_{out2} = a_1 \cos(\varphi - 90^\circ) + a_2 \cos(2\varphi - 90^\circ) + a_3 \cos(3\varphi - 90^\circ)$$
- $p_{in} \rightarrow Amp1 \rightarrow p_{in}$ :

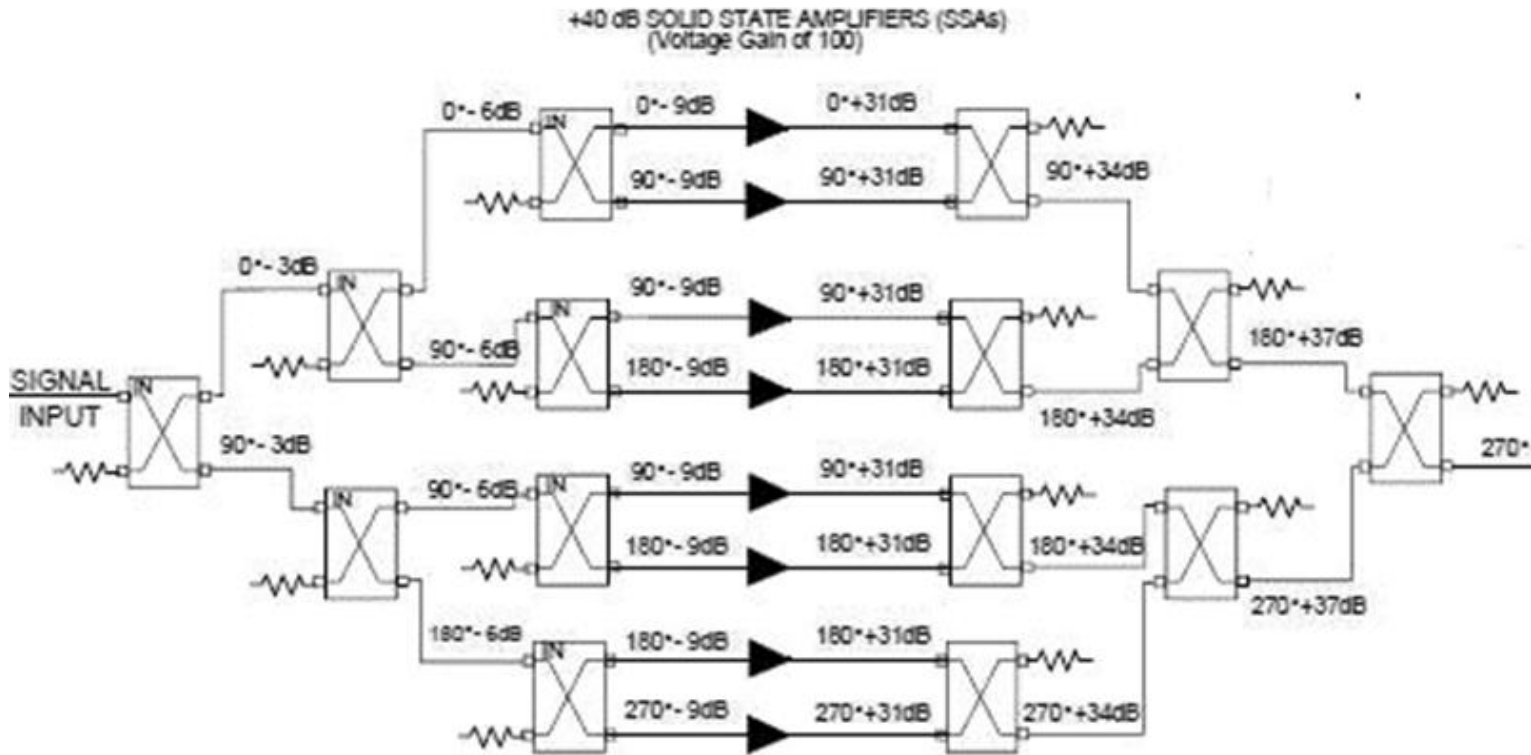
$$v_{out1} = a_1 \cos(\varphi - 90^\circ) + a_2 \cos(2\varphi - 180^\circ) + a_3 \cos(3\varphi - 270^\circ)$$
- Fundamental: in phase; H2:  $90^\circ$  out of phase; H3: out of phase

# Intermodulation in Quad Hybrid



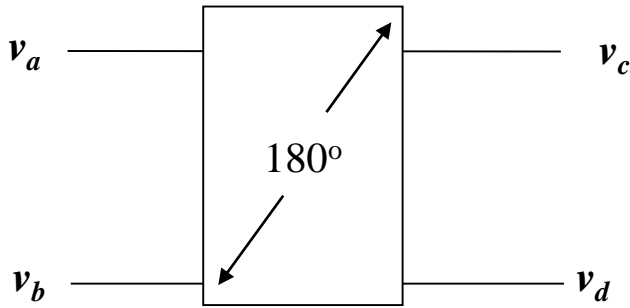
- IM2 (i.e.,  $p_{in}$  has two tones of  $f_a$  and  $f_b$ ) is 3dB lower in power
- IM3 of  $2f_a + f_b$  and  $f_a + 2f_b$  are cancelled.
- IM3 of  $2f_a - f_b$  and  $2f_b - f_a$  will add up in phase unfortunately, although we still have the original  $-6\text{dB}$  reduction from the lower output power in each amplifier.

# Hierarchical Quad Hybrid

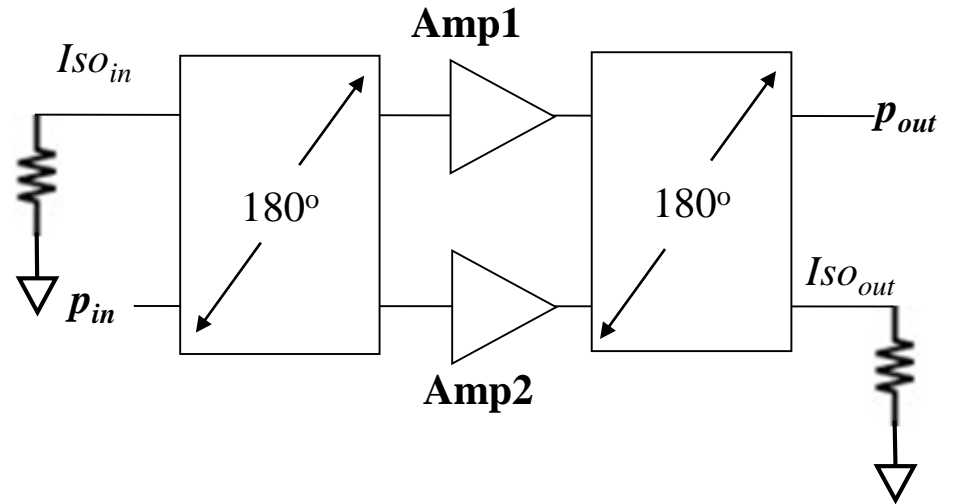


- We can repeat this module to achieve even better linearity.
- Combining 8 amplifiers to achieve 9dB reduction of  $v_{in}$  and  $v_{out}$  of each amplifier, while combined for the same  $p_{out}$
- This will have an effective reduction in IM3 by 18dB!!

# 180° Hybrid

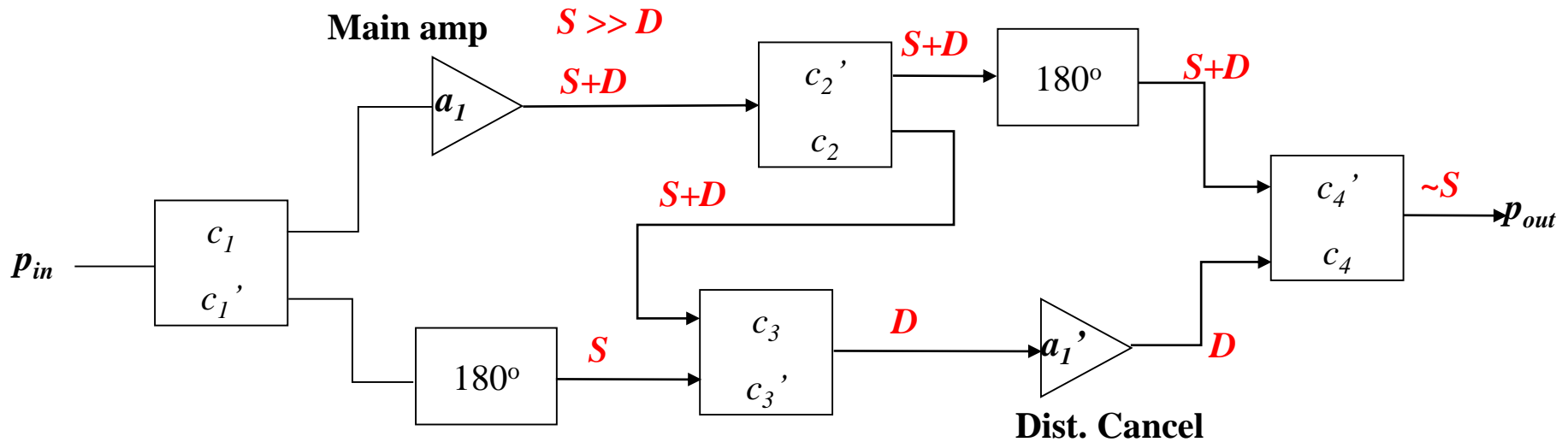


- $v_a$  is split to  $v_c$  and  $v_d$  both in phase with 3dB attenuation
- $v_b$  is split to  $v_d$  in phase with 3dB attenuation
- $v_b$  is split to  $v_c$  with  $180^\circ$  phase shift as indicated by the only arrow in the block



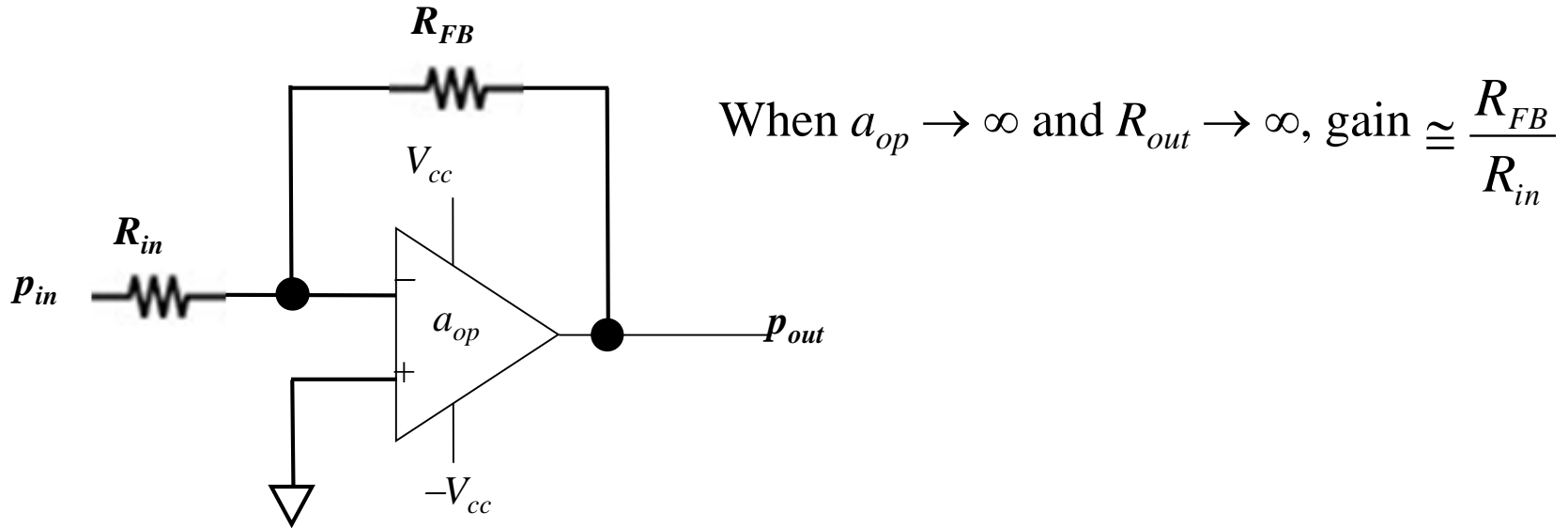
- For the fundamental frequency, the two paths to  $p_{out}$  will add up in phase, and will cancel at  $iso_{out}$  with  $180^\circ$  out of phase.
- Any impedance mismatch will cause some power subtracted from  $p_{out}$  to  $iso_{out}$ .
- H2, H3, IM2 and IM3?

# Feedforward Distortion Cancellation



- Main path:  $c_1 a_1 c_2' c_4'$  = Distortion eval path:  $c_1 a_1 c_2 c_3 a_1' c_4$
- Distortion sample path:  $c_1 a_1 c_2 c_3$  = Signal eval path:  $c_1' c_3'$
- Distortion cancellation:  $c_2' c_4' = c_2 c_3 a_1' c_4$   
 $c_1 a_1 c_2 c_3 = c_1' c_3'$
- $c_i + c_i' = 1$ , for  $i = 1 - 4$ .
- The main path gain to be maintained:  $c_1 \cong c_2' \cong c_4' \cong 1$ .
- Therefore, the real choices are just  $c_3$  and  $a_1'$ .

# Feedback Architecture



- Although LC resonators can be integrated into the OP AMP, the loop delay caused by the large Miller capacitance (as the OP AMP has huge gain) will limit the frequency range severely.

# Feedback Architecture Concerns

- **Huge distortion** (aka nonlinearity) when output voltage is close to  $V_{cc}$  or  $-V_{cc}$  of the OP AMP! Even many OP AMPs have  $V_{cc}$  from 10 – 24V, this is still just 30 dBm to 38 dBm of  $p_{out}$  on a  $50\Omega$  output resistance.
- The linear gain depends on the output load has much larger resistance than  $R_{FB}$  so that the gain is not heavily dragged down. However,  $R_{out}$  is mostly around  $50\Omega$ , which makes  **$R_{FB}$  and  $R_{in}$  to be very small and hence leaky.**
- We will either need a **matching network** or other circuit blocks to stabilize the linear gain.
- The power consumption at  $V_{cc}$  and  $-V_{cc}$ , and the leakage through  $R_{FB}$  and  $R_{in}$  can be serious, and the **power efficiency** is often very low without other resonance network.
- Not good for RF amplifiers, but probably good baseband amps.

# What Have You Learned?

- Components for RF signals splitting and combining
- Advantages of quad hybrids
- “Differential path architecture” can help linearity and impedance match
- Architecture to evaluate nonlinearity and apply cancellation