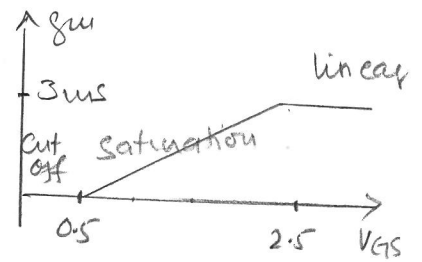


ECE Midterm Solutions (3150)

1a) $I_{D1} = k_n (V_{GS1} - V_{TN})$ Saturation } From Fig. $V_{TN} = 0.5 V$
 $= k_n V_{DS}$ Linear }



b) $V_{DS} = 0 \Rightarrow$ MOS Cap in inversion $C_{gs} = C_{ox} WL$

$\Rightarrow \frac{WL C_{ox}}{t_{ox}} = 172.5 \text{ fF} \Rightarrow t_{ox} = 20 \text{ \AA}$

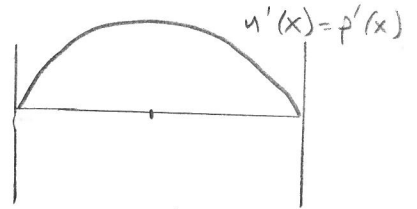
c) $\frac{dI_{D1}}{dV_{GS}} = k_n = \frac{W}{L} \mu_n C_{ox}$ } in Saturation $\Rightarrow \frac{W}{L} \mu_n C_{ox} = 1500 \mu A/V^2$
 $\Rightarrow \mu_n = 87 \text{ cm}^2/V\text{-s}$

2 a) $u'(0) = 0$ b) $p'(L) = 0$

c) $\frac{\partial^2 n'(x)}{\partial x^2} = -\frac{qL}{D_n}$ d) $n'(x) = -\frac{qL}{2D_n} (x-L)x$

e) $p'(x) = u'(x) = -\frac{qL}{2D_n} (x-L)x$

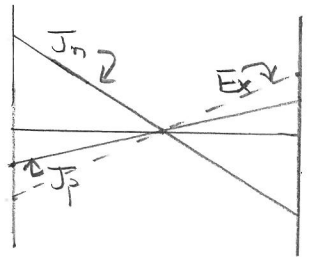
f) $J_n^{diff} = q D_n \frac{\partial n'}{\partial x} = -q q L (x - L/2)$



g) $J_n^{diff} = -q D_p \frac{\partial p'(x)}{\partial x} = +q \frac{D_p}{D_n} q L (x - L/2)$

h) $J_n^{diff} + J_p^{diff} + J_p^{drift} = J_T = 0 \Rightarrow J_p^{drift} = q \left(1 - \frac{D_p}{D_n}\right) q L \left(x - \frac{L}{2}\right)$

$J_p^{drift} = q \mu_p p_0 E = q \left(1 - \frac{D_p}{D_n}\right) q L \left(x - \frac{L}{2}\right)$

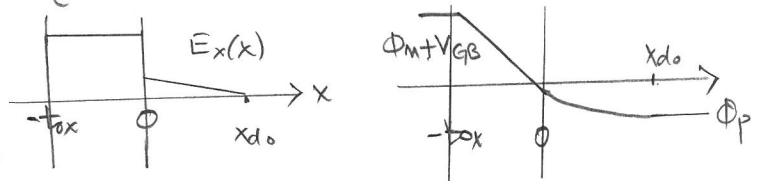


i) $I_L = A J_T = 0$

3 a) For $0 \leq x < x_{do}$ $E_x(x) = -\frac{q N_a}{\epsilon_s} (x - x_{do})$ as in the lecture notes.

At the oxide-sem interface $\epsilon_s E_x(x=0^+) - \epsilon_{ox} E_x(x=0^-) = Q_I$

$\Rightarrow E_x(x=0^-) = -\frac{Q_I}{\epsilon_{ox}} + \frac{q N_a x_{do}}{\epsilon_{ox}}$



b) For $0 \leq x \leq x_{do}$ $\phi(x) = \phi_p + \frac{q N_a}{2 \epsilon_s} (x - x_{do})^2$

For $-t_{ox} \leq x \leq 0$ $\phi(x) = \phi_p + \frac{q N_a x_{do}^2}{2 \epsilon_s} + \frac{Q_I}{\epsilon_{ox}} x - \frac{q N_a}{\epsilon_{ox}} x_{do} x$

c) Part (b) implies $\phi_B + V_{GB} = \frac{q N_a x_{do}^2}{2 \epsilon_s} - \frac{Q_I t_{ox}}{\epsilon_{ox}} + \frac{q N_a x_{do} t_{ox}}{\epsilon_{ox}}$

$x_{do} = 0$ when $V_{GB} = V_{FB} = -\phi_B - \frac{Q_I t_{ox}}{\epsilon_{ox}}$

4 a) $\frac{k_p}{2} (V_{out} - V_{DD} - V_{TP})^2 (1 - \lambda_p (V_{out} - V_{DD})) = \frac{k_n}{2} (V_{BIAS} - V_{TN})^2 (1 + \lambda_n V_{out})$

$k_p = k_n$ and $V_{out} = 1.5 \Rightarrow V_{BIAS} = 0.99 V$

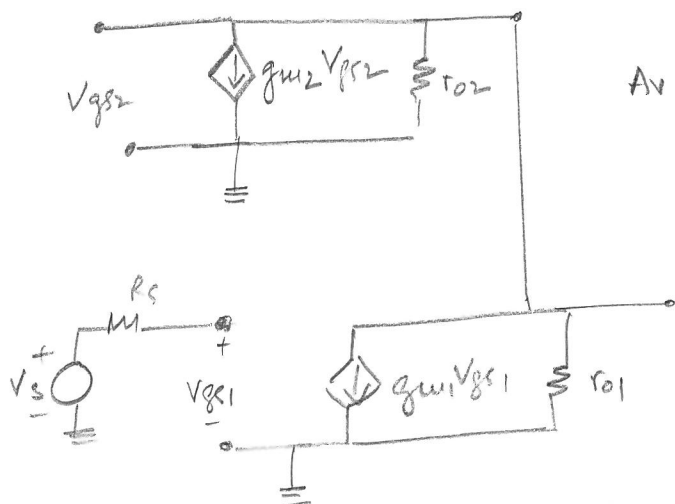
c) When V_{out} goes too low, $M1$ goes into linear region. Therefore

$$\frac{k_p}{2} (V_{out} - V_{DD} - V_{TP})^2 (1 - \lambda_p (V_{out} - V_{DD})) = \frac{k_n}{2} (V_{out})^2 (1 + \lambda_n V_{out})$$

$$\Rightarrow V_{out} \approx 1 \text{ Volt.}$$

b) Highest V_{out} can be calculated by seeing when $M2$ goes into cut-off. This happens when $V_{out} = 2.0 \text{ V}$.

d)



$$A_v = -g_{m1} (r_{o1} \parallel r_{o2} \parallel \frac{1}{g_{m2}})$$

$$\sim -\frac{g_{m1}}{g_{m2}} \sim -1 \quad (\text{small})$$

e) Looking in from the output node, $R_{out} = (r_{o1} \parallel r_{o2} \parallel \frac{1}{g_{m2}})$.

$$\sim \frac{1}{g_{m2}}$$