

1) a) $V_{BH} = V_H - V_{TN} = 2.5 \text{ V}$

b) $C_B \frac{dV_B}{dt} = I_D = \frac{k_n}{2} (V_H - V_B - V_{TN})^2$

c) $\int_0^{0.9V_{BH}} \frac{dV_B}{(V_H - V_B - V_{TN})^2} = \frac{k_n}{2C_B} \int_0^{t_{0 \rightarrow 1}} dt = \frac{k_n}{2C_B} t_{0 \rightarrow 1} \Rightarrow \frac{9}{V_{BH}} = \frac{k_n}{2C_B} t_{0 \rightarrow 1} \Rightarrow t_{0 \rightarrow 1} = 1.2$

d) $C_B \frac{dV_B}{dt} = -I_D = k_n \left(\frac{kT}{q}\right)^2 (m-1) e^{\frac{q(V_{TN} - V_B)}{mKT}} \left(1 - e^{-\frac{q(V_B)}{KT}}\right)$

Since $\left\{ \begin{matrix} V_B \gg \frac{kT}{q} \\ m = 2 \end{matrix} \right\} \Rightarrow \frac{dV_B}{dt} = -\frac{k_n}{C_B} \left(\frac{kT}{q}\right) e^{-\frac{qV_B}{2KT}}$

Integrating

$\Rightarrow V_B(t_2) - V_B(t=0) = -\frac{k_n}{C_B} \left(\frac{kT}{q}\right) e^{-\frac{qV_{TN}}{2KT}} t_L = -1 \text{ Volt} \Rightarrow t_L = 4.2 \text{ ms}$

2. a) $\Phi_B - V = \int E_x dx = 1.55 \text{ V} \Rightarrow \Phi_B = 1.55 - 0.8 = 0.75 \text{ V}$

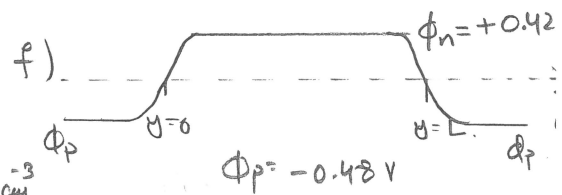
b) $C_j = \frac{\epsilon_s}{105 \text{ nm}} \cong 98 \text{ nF/cm}^2$ c) Since $\frac{dE_x}{dx} = +\frac{P(x)}{\epsilon_s} = 0$ for $0 < x < 5 \text{ nm}$

\Rightarrow no dopant in this range. d) $\epsilon_s \frac{dE_x}{dx} = P(x) = 4.14 \times 10^5 \text{ C/m}^3$

\Rightarrow +ve depletion charge density \Rightarrow N-type dopant $\Rightarrow N_d = \frac{4.14 \times 10^5}{q} = 2.58 \times 10^{24}$

$\Rightarrow N_d = 2.58 \times 10^{18} \text{ /cm}^3$

c) Flatband $\Rightarrow P(x=0) = \frac{n_i^2}{n(x=0)} = \frac{n_i^2}{N_d} = 10^3 \text{ /cm}^3$



g) At threshold $P(x=0) \cong N_d \Rightarrow n(x=0) = \frac{n_i^2}{P(x=0)} = \frac{n_i^2}{N_d} = 10^3 \text{ /cm}^3$

[Coulombs per unit area]

h) $Q_p = -C_{ox} [V_{GS} - V_{TP} - V_{CS}(y)]$ when $V_{DS} = 0$ $V_{CS}(y) = 0$ when $V_{DS} = -\Delta V_{DS}$

then $V_{CS}(y) \approx -\Delta V_{DS} \frac{y}{L} \Rightarrow V_{CS}(y=0) = 0$ + $V_{CS}(y=L) = V_{DS} = -\Delta V_{DS}$

Total inversion charge Q_p [Coulombs] = $-WC_{ox} \int_0^L dy [V_{GS} - V_{TP} - V_{CS}(y)]$

= $-WC_{ox} (V_{GS} - V_{TP})L - WC_{ox} \Delta V_{DS} \frac{L}{2} \Rightarrow \Delta Q_p = -\frac{WL}{2} C_{ox} \Delta V_{DS}$

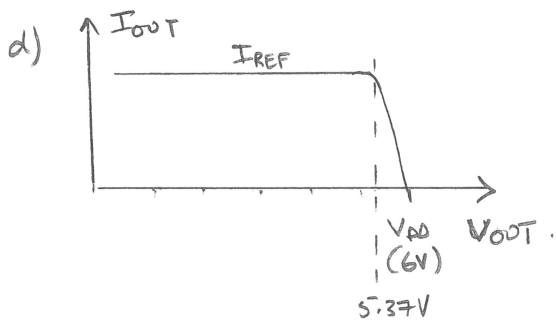
$\Rightarrow C_{gd} = \frac{-\Delta Q_p}{\Delta V_{DS}} = \frac{WL C_{ox}}{2}$

3 a) $\frac{k_p}{2} (V_a - V_{DD} - V_{TP})^2 = I_{REF} = 100 \mu A \Rightarrow V_a = 5 V$

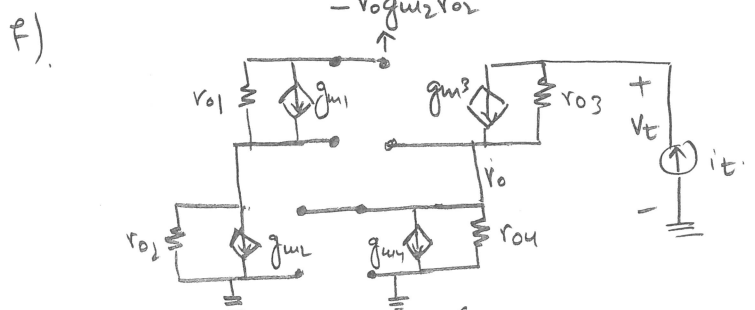
$\Rightarrow V_a - V_{DD} = V_b - V_a \Rightarrow V_b = 4 V$

b) $V_{OUT} > V_b - V_{TP} \Rightarrow V_{OUT} > 4.5 V \Rightarrow$ when $V_{OUT} > 4.5 V$ M3 will go into linear region.

c) Let the voltage at the source of M3 be V_0 . When $V_0 > V_a - V_{TP} = 5.5 V$ then M4 goes into linear region. At that point, M3 is already in the linear region so $I_{out} = k_p (V_b - V_0 - V_{TP} - (\frac{V_{OUT} - V_0}{2})) (V_{OUT} - V_0) = -I_{D3}$ but this must also equal $100 \mu A$ since M4 is in saturation (or at the border b/w linear + saturation regime). Putting $V_0 = 5.5 V$ gives $V_{OUT} = 5.37 V$. So if $V_{OUT} > 5.37 V$ M4 will go into linear region.



e) $R_{out} = r_{o3} + r_{o4} + g_{m3} r_{o3} r_{o4}$. (output resistance of a Cascode)



$V_0 = \frac{i_t}{g_{m4}} \Rightarrow V_t = V_0 + [i_t + g_{m3} (1 + g_{m2} r_{o2}) V_0] r_{o3} = i_t \left\{ r_{o3} + \frac{g_{m3}}{g_{m4}} r_{o3} + \frac{g_{m3}}{g_{m4}} g_{m2} r_{o2} r_{o3} \right\}$

4 a) $\frac{k_{p1}}{2} (V_a - 5 - V_{TP})^2 = 200 \mu A \Rightarrow V_a = 4 \text{ Volts}$

b) In common mode $V_s \approx V_{ic+1} \Rightarrow$ M3 will go linear if $V_s > V_a - V_{TP} \Rightarrow$ when $V_{ic} > 3.5 V$

c) $V_{o1} = V_{o2} = 100 \mu A \times R = 2 V$, M1 + M2 will go linear if $V_{o1} > V_{ic} - V_{TP}$ or $V_{ic} < V_{o1} + V_{TP} = 1.5 V$

d) $A_{vd} = -g_{mp} (r_{op} || R)$ e) current magnitude is $g_{mp} \frac{V_{id}}{2}$ and current will flow from node V_{o2} to node V_{o1} if $V_{id} > 0$

f) Small signal circuit is symmetric \Rightarrow half-circuit is a CS stage and $R_s = 0 \Rightarrow A_{vd} = -g_{mp} (R || r_{op}) \left\{ \frac{1 - j\omega \frac{C_{gd}}{g_{mp}}}{1 + j\omega C_{gd} (r_{op} || R)} \right\} \Rightarrow \omega_H = \frac{1}{C_{gd} (r_{op} || R)}$